A Review of Various Non-Emission Reduction Methods in Marine Diesel Engines

Anuar Abu Bakar¹, Sheikh Alif Ali^{1,}Mohammed Ismail Russtam Suhrab^{2*}, Mohammad Abdullah Abu Sayed³, Wan MohdNorsani Wan Nik¹, Wan Nurdiyana Binti Wan Mansor¹

¹ Faculty of Ocean Engineering Technology and Informatics, University Malaysia Terengganu, 21030 Kuala Nerus, Terengganu, Malaysia.

^{2*} Faculty of Maritime Studies, University Malaysia Terengganu, 21030 Kuala Nerus, Terengganu, Malaysia

³Research Scholar, FCT Nova, Industrial Engineering, Portugal Corresponding author: m.ismail@umt.edu.my

Abstract

NO_x has been described as one of the most harmful gases produced under high-temperature conditions from combustion chambers of marine diesel engines. Researchers have stressed the adverse effects of marine diesel engine emissions on human health and other biological systems. The International Convention on the Prevention of Pollution from Ships (MARPOL Annex VI) established NOx global emission limits. It provided a platform to encourage technological innovations toward reduction in NO_x emissions. Several specialized methods have been in application for NOx emission reductions, but their operational processes and technical efficiencies remain poorly understood. Therefore, a comprehensive review has been conducted on various NO_x emission reduction methods, classified into primary and secondary methods. The formation process of NOx was assessed in detail, and the multiple methods in application toward NO_x emission reduction were evaluated based on their technological efficiencies. It was established that scavenge humidification and SNCR- selective noncatalytic reduction is the most efficient NOx emission reduction method, given their emission reduction potentials at 80% and 95%, respectively.

Keywords: marine diesel engine; emission; humidity.

Introduction

International trades and logistical operations worldwide mainly rely on shipping as a transportation medium. United Nations Conference on Trade and Development (UNTAD) reported in 2019 that global sea trade accounted for more than 11 billion tons of trade. There has been reported an increase in the number of merchant ships in operation worldwide with immense negative impacts on the environment and human health ^{1,2}. Ships transport large quantities of essential goods through the world's oceans and emit high and varying quantities of nitrogen oxides (NO_x), which are detrimental to the environment.NO_x gas is a harmful gaseous emission released into the environment and, upon reaction in the atmosphere, forms photochemical smog^{3,4}. The Committee on the Protection of Marine Environment (MEPC) is under International Maritime Organization (IMO). The Committee is responsible forthe regulatory framework developed to prevent air pollution under The International Convention for the Prevention of Pollution from Ships (MARPOL) Convention, Annex VI Regulations

(13.8 and 5.3.2) of NO_x Technical Code 2008^{5-7} . There have been reported cases of non-compliance to regulations and existing laws aimed at reducing ships' emissions of NO_x pollutants. In this paper, various NO_x emission reduction methods in marine diesel engines have been comprehensively reviewed. This was to provide the most updated knowledge on NO_x emissions reduction technologies, assess the technical efficiency of the technologies, and offer recommendations for necessary improvements.

Nitrogen Oxides Pollutants

Fossil fuels are subjected to combustion for power generation in marine diesel engines, thus releasing greenhouse gases considered very harmful to the environment⁸. Typical emission contains primary greenhouse gases such as methane (CH₄), NO_x, and carbon dioxide (CO₂)⁹. NOx is a term for a group of predominantly nitric oxide (NO) with small percentages of nitrogen dioxide (NO₂) and nitrous oxide (N₂O)11. In atmospheric chemistry, the nitrogen concentration in natural air is about 79.05%10. Nitrogen remains inactive mainly in the marine diesel engine combustion process. However, a small part is oxidized to form NO_x pollutants¹². During the combustion process in marine diesel engines, NO_x is included within the burning fuel spray under high combustion temperature conditions, providing an avenue for the reaction of nitrogen and oxygen to form nitric oxide (NO) and nitrogen dioxide (NO₂)¹³. More NO_x is included in the chamber at high temperatures and longer residence time. The quantity of NO_x reaches a maximum amount when the actual fuelair ratio becomes close to the stoichiometric value¹⁴. NO_x formation occurs within 20° of the crank's rotation after the beginning of combustion in the marine diesel engine—NO_x forms as both front-propagated flame and post-flame gases. However, at high-pressure combustion conditions in marine diesel engines, the flame reaction zone becomes very thin and shortens flame residence time in the zone¹⁵.

Primary sources of NO_x Pollutants

Many researchers have reported on the formation of NO_x at high-temperature conditions, like at temperatures greater than 1800K; diatomic nitrogen is formed following air oxidation in marine diesel engine combustion chamber 16,17 . The thermal NO_x trail occurs at high gas temperature conditions, and under this condition, thermodynamic steadiness favors (NO) formation through molecular nitrogen and oxygen dissociations 18,19 . The strong triple bond in the N_2 molecule requires high temperature for breaking its radicals into $N_2 \rightarrow 2N$ and $O_2 \rightarrow 2O$, and NO_x is also produced naturally by lightning. According to Zeldovich's mechanisms, thermal NO_x requires high activation energy and is quickly formed at high temperatures, as shown in Eq 1-3 20 . The most important for a stoichiometric and lean premixed combustion (a thermal mechanism) occurs where temperatures are more significant than 1527 $^{\circ}$ C. The NO_x creation process, known as hot spots, is very nonlinear since there are regions of higher temperatures above average temperature, and they play a more significant role in determining the produced amount of NO_x . NO can also disintegrate to form N_2 and O_2 . However, this happens seldomly. Thus, almost all of the NO_x emitted is NO_x , which is equally described as a thermal effect 21,22 .

$N_2+O \rightarrow NO+N$	(Eq. 1)
$N+O_2 \rightarrow NO+O$	(Eq. 2)
$N+OH\rightarrow NO+H$	(Eq. 3)

Fuel NO_x contributes to the oxidation of volatile nitrogen contained in fossil fuel at initial combustion phases before the reaction of volatile nitrogen to form intermediaries that are oxidized into NO or exist freely as N₂ for release into the atmosphere. Fuel NO_x can produce 50% and 80% of total emissions through fossil fuel and coal combustions, respectively, and this has been described as a dilution effect²³. Prompt NO_x refers to the reaction between atmospheric nitrogen, N₂, and radicals of fossil fuel (CH₂, CH, and C fragments) for the formation of fixed species of nitrogen comprising nitrogen monohydride (NH), hydrogen cyanide (CHN), dihydrogen cyanide (H₂CN) and chloroacetophenone (CN or CN gas), that is liable to oxidation to form NO. Prompt NO_x is in minimal concentration in fossil fuels containing nitrogen, which has equally been described as a chemical effect.

Primary and Secondary NO_x Pollutants Reduction Methods

Several emission reduction methods have been identified and associated with different technical and operational challenges. Primary NO_x reduction methods focus on reducing emission components' production at the combustion phase of fossil fuels through controlling combustion processes, lowering oxygen-nitrogen concentrations, and reducing associated combustion temperature21. Secondary treatment technologies do not focus on combustion engines and boilers' working operations but target emission reduction associated with land-based stationary sources later converted or "marinized" for onboard usage ships. Operators' compliance with NO_x emission limits is becoming challenging, associated with a considerable cost, and regulations that limit emissions are becoming stricter.

Fuel Blending for NO_x Pollutants Reduction

The mixture of hydrocarbon composites (ethane, methane, etc.) and diesel causes the lowering of cetane numbers and reduced flame temperature due to increased flame ignition delay²⁴. Another study reported that the absorption of combustion released heat energy, causing the evaporation of hydrocarbon compounds with high latent heat, leading to a decrease in flame temperature²⁵. It has been claimed in several types of research that the use of blended Fuel in marine diesel engines has the potential to reduce NO_x emission²⁶⁻²⁸. Blended Fuel potentially lowers combustion heating value and particulate matter to about 75%²⁹. Due to the constant amount of carbon, several experiments have demonstrated that blended Fuel has a significant effect on NO_x reduction^{30,31}. It has been reported that different additives can be used in blended Fuel as a catalyst to reduce peak combustion temperature³²⁻³⁴

Exhaust Gas Recirculation

Exhaust gas recirculation (EGR) technology has been reported as another technique deployed to reduce NOx emission35,36 efficiently. EGR uses a turbochargerto recycle exhaust gas, significantly reducing NOx emission³⁷⁻³⁹. EGR is recommended for application in low-speed marine diesel engines and operates from the turbine side downstream of the

turbocharger to the compressor inlet of the engine⁴⁰. Low-speed marine diesel engines are driven by heavy fuel oil (HFO), which produces heavily laden sulphur, metals, and other components in the exhaust gas. These components must be eliminated from the exhaust gas before its recirculation into the scavenge space of the marine diesel engines¹⁸.EGR has been considered inappropriate for engines using HFO due to challenges associated with cleaning the exhaust gas before recirculation. Despite this, EGR is still being recommended for use by top manufacturers of marine diesel engines (Wartsila, MAN Diesel, and Mitsubishi), especially for HFO fuel using engines with inbuilt scrubber systems. In early 2011, MAN Diesel manufacturer claimed that EGR technology could reduce NO_x emission to 50 or 60%. NO_x emission reduction was driven by adding CO₂ into combustion air to decrease peak combustion temperature owing to the high specific gravity of CO₂ in comparison to air^{33,41-44}. EGR emission reduction technology remains increasingly utilized in main propulsion and auxiliary engines of board ships⁴⁵. The technology, as claimed, can reduce NO_x emission levels to about 60% and equally has the potential to reduce emissions during sea passage and port stay.

Slide Fuel Valve

The fuel injector slide valve was used by industry and regulators as a green engineering piece to reduce NO_x emission even to 20 years old marine diesel engines. The nozzle design of the slide fuel valve has been redesigned by eliminating a minute channel (sac volume) which retains a small amount of Fuel after injection. The retained Fuel drips into the engine combustion chamber and burns incompletely. SAC located within valve seating is referred to as the small volume between the fuel injector's fuel flow path and the injector's final metering of the injector⁴⁶. This technology improved engine efficiency and cylinder condition. Slide valve strategy is specific to MAN B&W 2-stroke slow-speed engines mainly used for ship propulsions and, in 2004, was built into all new MAN B&W two-stroke engines. The main advantages of this system include reduced fuel consumption due to complete removal of (SAC) volume, NO_x reduction potential at about 30%, and dependence on operational load⁴⁷.

Miller Cycle (Dynamic/Variable Valve Actuation)

The Miller cycle represents the Otto Cycle's modification from shorteningthe compression stroke followingthe expansion stroke to reducing fuel consumption and exhaust gas emissions with the inclusion of NO_x⁴⁸. The Miller cycle utilizes variable valve actuation (VVA) and advanced turbocharging systems for NO_x emission reduction in marine diesel engines. The main advantage of the Miller cycle is the reduction of fuel consumption by the consistent guarantee of the expansion ratio being more significant than the compression ratio. Research has shown that the Miller cycle's early inlet valve closure (EIVC) system utilizes high values of boosted air pressure through two-stage turbocharging compared to conventional marine diesel engine operations⁴⁹. Extreme values of EIVC in conjunction with increased boost pressure resulted in a remarkable emission reduction of engine NO_x up to 50% without deterioration of brake-specific fuel consumption (BSFC)^{50,51}.

Split Fuel Injection

Split fuel injection,referred to as premix charged compression ignition, is known for its single-stage combustion process. Large fuel volumes are burnt, reducing cylinder temperature, unlike normal compression ignition engines. In split fuel injection, combustion occurs after some injection timing variations and guaranteed proper fuel-air mixture⁵². Another study reported that injections into the engines lower the combustion temperature and pressure, and a significant reduction in NOx emission is recorded with a split injection system compared to that of single injection^{53,54}.

Fuel Emulsion System

A fuel emulsion system houses two immiscible fluids (e.g., water and diesel) whereby one of the fluids is in fine dispersion in the combustion chamber; like in a water/diesel fuel emulsion system, water is found to be in continuous dispersion as fine droplets in the diesel fuel. [70-75] Previous studies reported that water in the emulsion system is liable for a reduction in combustion temperatures⁵⁵⁻⁵⁷. In another study, the researchers have established that using a water-fuel emulsion system could reduce NO_x emission to about 50%, with every 1% of water utilized, accounting for a corresponding percentage point of NOx emission reduction⁵⁸. Using afuel emulsion system without engine modifications could lead to the maximum amount of water and decreased emission quantity of NO_x being limited to about 10 - 20%. The engine can equally not meet its rated power output^{56,59}. Using water in the fuel emulsion system improves the combustion efficiency of CI engines and overall enhances engine performance. A percentage increase of water in the emulsion system up to about 20% will increase the motor torque, power, and brake thermal efficiency. The brake-specific fuel consumption (BSFC) is determined by some critical variables like the total Fuel utilized, burnt quantities of diesel fuel, and exhaust gas temperature known to be decreased with increasing water percentage^{60,61}.

Direct Water Injection

Direct Water Injection (DWI) is a well-established technology. This technology has the potential for NO_x emission reduction of up to 50% and is considered deployable for main propulsion and auxiliary engines61. Still, it is associated with limited usage on board ships due to Fuel's extremely high sulphur content exposed to acidic attack on the engine piston crown. The introduction of water into the combustion system of the marine diesel engine has been described as a NO_x emission reduction strategy and simultaneously reduces PM emissions. Another researcher described water injection as internal cooling, and fully independent water injection is required for in-cylinder injection of the water system^{62,63}. This direct water injection method provides the platform for water injection in large quantities without impacting negatively on the diesel engine reliability, and previous studies reported that injection timing, water consumption, NOx emission, and other parameters could be subjected to careful optimization for enhanced efficiency of the direct water injection system⁶⁴⁻⁶⁶.

Scavenge Humidification

This requires the introduction of water mist into a scavenging system and has been described as one of the simplest techniques for water displacement into an engine combustion chamber⁶⁷. This technique has been in application for several decades and is designated for boosting power and preventing the knocking of SI engines⁶⁸. Water mist can be generated from engine waste heat in the exhaust gas or compressed scavenging air. Steam can be used in place of water mist in certain engine applications^{69,70}. The integration of steam injection systems into diesel engines has shown that the combustion temperature will decrease as the vapor in the steam increases. Some researchers have concluded that steam injection could reduce the concentration of CO and CO₂ emission⁷¹. The water or steam injection method was normally applied to in-flight engines, but in recent years, the research on diesel and gasoline engines has been extended⁷². Research has shown that the water injection method is very efficient since it can account for more than 80% reduction in NO_x emission as reported by^{67,73}.

Selective Catalytic Reduction

Selective Catalytic Reduction (SCR) has demonstrated a strong capacity to reduce marine diesel engines' NO_x emissions. This has resulted in several companies being involved in SCR solutions manufacturing⁷⁴. SCR requires the treatment of exhaust gases with ammonia or urea before being fed through a catalytic converter at temperatures above 250°C to break down NOx into water and nitrogen. SCR's efficiency is known to be limited by temperature. At low exhaust temperatures, hydrogen sulfate is formed with a great tendencyto cause operational obstructions to the catalytic converter. SCR requires special space requirements, which must have urea system storage for potential reduction of NO_x emission. Following the history of engine operations at port areas, engine temperatures decrease in the transition and maneuvering modes, with high exhaust temperatures going below 250°C. Integrating scrubber or waste heat recovery systems into the SCR technology is responsible for the drop in exhaust temperature below 250°C, which does not guarantee the operational efficiency of the SCR system. The efficiency of the SCR is equally impacted by high sulphur content fuel, which may be used in the marine diesel engine 75. Most SCR systems are installed on 4-stroke diesel engines, and their applicability is limited to 2 stroke main propulsion engines.

Exhaust Gas Scrubber

An exhaust gas scrubber (EGS) functions by the removal of sulphur and PM through a dry or wet scrubbing interface from the exhaust flow of the engine. One of the main advantages of sulphur stripping from the exhaust gas is that the ship can use high sulphur fuels and meet the requirements of the IMO and Emission Control Area (ECA)⁷⁶⁻⁸⁰. There are two types of scrubbers, namely dry and wet scrubbers, with the most used being the wet scrubbers of different configurations (open-loop, closed-loop, and hybrid). Open-loop systems utilize seawater; closed-loop uses freshwater, while seawater-freshwater combinations apply to the hybrid configuration. In open-loop wet scrubber systems, exhaust gases are sprayed with seawater, leading to the reaction of SO_x with wash water to form sulphuric acid, which becomes neutralized by the natural alkalinity of seawater. Seawater

serves as the wash water in the system, and the wash water is subjected to treatment after utilization in the scrubber. Then, the Closed-loop scrubber systems on board freshwater are utilized and subjected to mixing with caustic soda (NaOH) to serve as wash water. It remains very uncertain if port permits are required to discharge scrubber effluents in confined waters of port areas. It has the potential for 98% and 5% reductions in SO_x and NO_x emissions, respectively.

Conclusion

The following was detected whilereviewing recent progress in water/steam addition to fluids combustion systems. Few studies have investigated the various methods. The current research situation in this field leads to the following findings:

- 1. It has been established that scavenge humidification has the potential for NOx reduction to greater than 65%, associated with lower operating cost, and provides opportunities for future Improvement compared to others. However, the requirement for special water quality and high tendencies of corrosion attacks remained the major drawbacks of scavenging humidification.
- 2. SCR has the potentiality of NO_x emission reduction to 95% through ammonia injection into the exhaust gas system. The implementation of some special operations, as recommended, will have a positive influence on NOx emission control expenditures and the temperature needs of SCR. However, the main drawbacks remained the high catalyst cost, high-temperature requirement, and short catalyst service life.
- 3. It can be noted that the commercial applicability for direct water injection in liquid Fuel-burning for low-NOx technologies has not yet been proved. Further, when using different types of standard fuels and wastes with a particular focus on alternative uses of those fuels in developing sustainable energy, thermal-physical effects and chemical kinetics of water injection should be studied on combustion features and emissions.
- 4. When liquid Fuel is burned with the steam injectors, NOx can be reduced by 34% following current environmental regulations with a high level of fuel consumption and low carbon monoxide CO concentration (EN:267).
- 5. The efficiency reduction of NOx depends on a range of parameters, including steam levels, jet speeds, injection site, and delivery mechanism. Excess humidity may have a negative impact on the combustion process in the combustion zone, creating effects like excessive cooling of the combustion chamber, flame extinguishing, fuel under-burning, CO rise, etc. Specific applications, therefore, require different studies.
- 6. Moisture effects on liquid fuel combustion NOx emissions in burners are determined by two basic mechanisms: chemical and physical. The first Impact is to raise the concentration of active hydroxyl radicals that effectively oxidizeblack carbon precursors in steam injection into the combustion zone, boosting carbon fuel burnout and minimizing the number of harmful combustion products. The second Effect is related to the fuel mixture and steam dilution, reducing the flame temperature and thermal NOx concentration.
- 7. Moisture for combustion can be autonomously generated from the combustion heat of Fuel, i.e., no additional energy sources are necessary. Thus, combustion technologies may be applicable in remote areas where high-quality fuels cannot produce thermal and electrical

energy. Nonetheless, there is still a large build-up of unused industrial and transportable fuel waste.

Acknowledgment

Any grant did not fund this research.

Conflict of Interest

The authors declare that they have no conflict of interestconcerning the research.

Authors Contribution

All authors contributed in this research paper.

References

- [1] Onofri M, BernabeoR A & Webster K, Health and environmental impacts of NO_x: An ultra-low level of NO_x(nitrogen oxides) achievable with anew technology, *GlobJ EngSci*, 2(3), (2019). https://doi.org/10.33552/GJES.2019.02.000540.
- [2] Baldean D, Andrei L& Borzan A I, Research of NO_x and PM₁₀ pollutants in Cluj-Napoca with the mobile system for mitigating public health risks, *IOP Conf S Mater Eng*, 898, 012003 (2020). https://doi.org/10.1088/1757-899X/898/1/012003.
- [3] Skowron A, Lee D S, León R R D, Lim L L& Owen B, Greater fuel efficiency is potentially preferable to reducing NO_x emissions for aviation's climate impacts, *NatCommun*, 12 564, (2021). https://doi.org/10.1038/s41467-020-20771-3.
- [4] Li J, Li H, Wang X, Wang W, Ge M, *et al.*, A large-scale outdoor atmospheric simulation smog chamber for studying atmospheric photochemical processes: Characterization and preliminary application, *J Environ Sci*, 102 (185-197), (2021). https://doi.org/10.1016/j.jes.2020.09.015.
- [5] International Maritime Organization (2008). Amendments to the technical code on control of emission of nitrogen oxides from marine diesel engines, page 1-100. Retrieved from https://www.cdn.imo.org/localresources/en/KnowledgeCentre/IndexofIMOResolutions/MEPC Documents/MEPC.177(58).pdf.
- [6] International Maritime Organization (2017). 2017 guidelines for the development and management of the IMO ship fuel oil consumption database, pages 1-6. Retrieved from https://www.classnk.or.jp/hp/pdf/activities/ statutory/seemp/seemp-mepc293-71.pdf.
- [7] International Maritime Organization (2017). 2017 guidelines for administration verification of ship fuel oil consumption data. Retrieved from https://www.liscr.com/sites/default/files/liscr_imo_resolutions/ Res.292_71_pdf.pdf.
- [8] Ko B H, Hasa B, Shin H, Jeng E, Overa S, *et al.*, The Impact of nitrogen oxides on electrochemical carbon dioxide reduction, *Nature Commun*, 11 5856, (2020). https://doi.org/10.1038/s41467-020-19731-8.
- [9] Sharaf J, Exhaust emissions and its control technology for an internal combustion engine, *Intern JEng ResAppl*, 3 (4), 947-960 (2013). https://www.ijera.com/papers/Vol3_issue4/FC34947960.pdf.

- [10] Zhu M, He C, Wu T, Liu Y, Guan Y, et al., Simulation for separation of oxygen and nitrogen from air, Frontiers Separ SciTechnol, 844-849 (2004). https://doi.org/10.1142/9789812702623_0162.
- [11] Rakopoulos C D, Kosmadakis G, Demuynck J, Paepe M D & Verhelst S, A combined experimental and numerical study of thermal processes, performance and nitric oxide emissions in a hydrogen-fueled spark-ignition engine, *Intern J Hydrogen Energ*, 36 (8), 5163-5180 (2011). https://doi.org/10.1016/j.ijhydene.2011.01.103.
- [12] Zare A, Stevanovic S, Jafari M, Verma P, Babaie M, *et al.*, Analysis of cold-start NO₂ and NO_x emissions, and the NO₂/NO_x ratio in a diesel engine powered with different diesel-biodiesel blends, *EnvironPollut*, 290, 118052 (2021). https://doi.org/10.1016/j.envpol.2021.118052.
- [13] Sharma T K, Rao G A P & Murthy k m, Effective reduction of NO_X emissions of a HCCI (Homogeneous charge compression ignition) engine by enhanced rate of heat transfer under varying conditions of operation, *Energ*, 93 (part 2), 2102-2115 (2015). https://doi.org/10.1016/j.energy.2015.10.083.
- [14] Jiang C, Li Z, Qian Y, Wang X, Zhang Y, *et al.*, Influences of fuel injection strategies on combustion performance and regular/irregular emissions in a turbocharged gasoline direct injection engine: Commercial gasoline versus multi-components gasoline surrogates, *Energ*, 157, 173-187 (2018). https://doi.org/10.1016/j.energy.2018.05.160.
- [15] Hagen L, Breaux B, Flory M, Hiltner J & Fiveland S, Experimental investigation of NO_x formation in a dual fuel engine, *J Eng Gas TurbinesPower*, 140 (12), 122802 (2018). https://doi.org/10.1115/1.4040179.
- [16] Jabbar T, Saleh I H & Dakhil S F, Influence radiative properties for the combustion chamber surface on thermal NO_x, *Journal Heat Mass Transfer*, 15 (3), 531-542 (2018). https://doi.org/10.17654/HM015030531.
- [17] Xiaohe X, Zhaomin L, Shilin Y, Houzhang T, Baixiang X, *et al.*, Coke preheating combustion study on NO_x and SO₂ emission, *JEnerg Inst*, 97, 131-137 (2021). https://doi.org/10.1016/j.joei.2021.04.007.
- [18] Hebbar G S, NO_x from diesel engine emission and control strategies A review, *InternJMech Eng Robotics Res*, 3 (4), 471-482 (2014). http://www.ijmerr.com/uploadfile/2015/0409/20150409042911754.pdf.
- [19] Mansor W N A, Abdullah S, Othman C W M N C W, Jarkoni M N K, Chao H R, et al, Data on greenhouse gases emission of fuels in power plants in Malaysia during the year of 1990-2017, Data in Brief, 30, 105440 (2020). https://doi.org/10.1016/j.dib.2020.105440.
- [20] Ismail M Y, Mamat R, Akasyah M K, Jamlos M A & Yusop A F, Evaluation of engine combustion and exhaust emissions characteristics using diesel/butanol blended Fuel, *Appl Therm Eng*, 156, 209-219 (2019). https://doi.org/10.1016/j.applthermaleng.2019.02.028.
- [21] Muzio LJ & Quartucy GC, Implementing NO_x control: Research to application, *Prog Energ Combust Sci*, 23 (3), 233-266 (1997). https://doi.org/10.1016/S0360-1285(97)00002-6.
- [22] Mansor W N W, Abdullah S, Jarkoni M N K, Vaughn J S&Olsen D B, Data on combustion, performance and emissions of a 6.8 L, 6-cylinder, Tier II diesel engine, *Data in Brief*, 33, 106580 (2020). https://doi.org/10.1016/j.dib.2020.106580.
- [23] Elkelawy M, Shenawy E A, Almonem S K A, Nasef M H, Panchal H, e *et al.*, Experimental study on combustion, performance, and emission behaviours of diesel/WCO biodiesel/

- Cyclohexane blends in DI-CI engine, *Process Saf Environ Prot*, 149, 684-697 (2021). https://doi.org/10.1016/j.psep.2021.03.028.
- [24] Bogarra M, Herreros J M, Tsolakis A, York A, Millington P J, *et al.*, Impact of exhaust gas fuel reforming and exhaust gas recirculation on particulate matter morphology in gasoline direct injection engine, *JAerosol Sci*, 103, 1-14 (2017). https://doi.org/10.1016/j.jaerosci.2016.10.001.
- [25] Szybist J P, Song J, Alam M & Boehman A L, Biodiesel combustion, emission and emission control, *Fuel Process Technol*, 88 (7), 679-691 (2007). https://doi.org/10.1016/j.fuproc.2006.12.008.
- [26] Wang X, Wang Y & Bai Y, Oxidation behaviors and nanostructure of particulate matter produced from a diesel engine fueled with n-pentanol and 2-ethylhexyl nitrate additives, *Fuel*, 288, 119844 (2021). https://doi.org/10.1016/j.fuel.2020.119844.
- [27] Wei L, Cheng R, Mao H, Geng P, Zhang Y, *et al.*, Combustion process and NO_x emissions of a marine auxiliary diesel engine fuelled with waste cooking oil biodiesel blends, *Energ*, 144, 73-80 (2018). https://doi.org/10.1016/j.energy.2017.12.012.
- [28] Geng P, Mao H, Zhang Y, Wei L, You K, *et al.*, Combustion characteristics and NO_x emissions of a waste cooking oil biodiesel blend in a marine auxiliary diesel engine, *Appl Therm Eng*,115, 947-954 (2017). https://doi.org/10.1016/j.applthermaleng.2016.12.113.
- [29] Lin Y C, Hsu K H & Chen C B, Experimental investigation of the performance and emissions of a heavy-duty diesel engine fueled with waste cooking oil biodiesel / ultra-low sulfur diesel blends, *Energ*, 36 (1), 241-248 (2011). https://doi.org/10.1016/j.energy.2010.10.045.
- [30] Venu H, Raju V D, Lingesan S &Soudagard M E M, Influence of Al₂O₃nano additives in ternary Fuel (diesel-biodiesel-ethanol) blends operated in a single cylinder diesel engine: Performance, combustion and emission characteristics, *Energ*, 215 (Part B), 119091 (2020). https://doi.org/10.1016/j.energy.2020.119091.
- [31] Rafał Smolec, Marek Idzior, Wojciech Karpiuk, and Miłosław Kozak. "Assessment of the potential of dimethyl ether as an alternative fuel for compression ignition engines". *Combustion Engines* 169 (2), 181-186 (2017). https://doi.org/10.19206/CE-2017-232
- [32] Subramanian T, Varuvel E G, GanapathyS, Sivasankaralingam V & Raman V, Role of fuel additives on reduction of NO_x emission from a diesel engine powered by camphor oil biofuel, *Environ SciPollut Res*, 25 (32), 15368-15377 (2018). https://doi.org/10.1007/s11356-018-1745-4.
- [33] Hanafi H, Hasan M, Rahman M, Noor M, Kadirgama K *et al.*, Numerical modeling on homogeneous charge compression ignition combustion engine fueled by diesel-ethanol blends, *MATEX Web of Conferences*, 74, 00037 (2016). https://doi.org/10.1051/matecconf/20167400037.
- [34] Yusof S N A, Sidik N A C, Asako Y, Japar W M A A, Mohamed S B, et al., A comprehensive review of the influences of nanoparticles as a fuel additive in an internal combustion engine (ICE). Nanotechnologiey Rev, 9 (1), 1326-1349 (2020). https://doi.org/10.1515/ntrev-2020-0104.
- [35] Venu H, Subramani L & Raju V D, Emission reduction in a DI diesel engine using exhaust gas recirculation (EGR) of palm biodiesel blended with TiO₂ nano additives, *Renew Energ*, 140, 245-263 (2019). https://doi.org/10.1016/j.renene.2019.03.078.

- [36] Chen G, Di L, ZhangQ, Zheng Z & Zhang W, Effects of 2,5-dimethylfuran fuel properties coupling with EGR (exhaust gas recirculation) on combustion and emission characteristics in common-rail diesel engines, *Energ*, 93 (part 1), 284-293 (2015). https://doi.org/10.1016/j.energy.2015.09.066.
- [37] Verhelst S, Vancoillie J, Naganuma K, Paepe M D, Dierickx J, et al., Setting a best practice for determining the EGR rate in hydrogen internal combustion engines, Intern J Hydrogen Energ, 38 (5), 2490-2503 (2013). https://doi.org/10.1016/j.ijhydene.2012.11.138.
- [38] Jamsran N, Park H, Lee J, Oh S, Kim C, *et al.*,Influence of syngas composition on combustion and emissions in a homogeneous charge compression ignition engine,*Fuel*, 306, 121774 (2021). https://doi.org/10.1016/j.fuel.2021.121774.
- [39] Zhou L, Study on EGR technology routes of vehicle engine A review, *Adv MaterRes*, 805-806, 1416-1420 (2013). https://doi.org/10.4028/www.scientific.net/AMR.805-806.1416.
- [40] Sakhare N M, Shelke P S & Lahane S, Experimental investigation of Effect of exhaust gas recirculation and cottonseed B20 biodiesel fuel on diesel engine, *Procedia Technol*, 25, 869-876 (2016). https://doi.org/10.1016/j.protcy.2016.08.195.
- [41] Qi D, Ma L, Chen R, Jin X & Xie M, Effects of EGR rate on the combustion and emission characteristics of diesel-palm oil-ethanol ternary blends used in a CRDI diesel engine with double injection strategy, *Appl Therm Eng*, 199, 117530 (2021). https://doi.org/10.1016/j.applthermaleng.2021.117530.
- [42] You J, Liu Z, Wang Z, Wang D & Xu Y, Experimental analysis of inert gases in EGR on engine power and combustion characteristics in a stoichiometric dual fuel heavy-duty natural gas engine ignited with diesel, *Appl Therm Eng*, 180, 115860 (2020). https://doi.org/10.1016/j.applthermaleng.2020.115860.
- [43] Yan B, Wang H, Zheng Z, Qin Y & Yao M, The effects of LIVC Miller cycle on the combustion characteristics and thermal efficiency in a stoichiometric operation natural gas engine with EGR, *Appl Therm Eng*, 122, 439-450 (2017). https://doi.org/10.1016/j.applthermaleng.2017.04.121.
- [44] Wei H, Zhu T, Shu G, Tan L & Wang Y, Gasoline engine exhaust gas recirculation A review, *Appl Energ*, 99, 534-544 (2012). https://doi.org/10.1016/j.apenergy.2012.05.011.
- [45] Epping K, Aceves S, Bechtold R & Dec J E, The potential of HCCI combustion for high efficiency and low emissions, *SAE Tech Pap 2002-01-1923* (2002). https://doi.org/10.4271/2002-01-1923.
- [46] Chang M, Park J, Kim B, Park J H, Park S, *et al.*, Effect of sac-volume on the relationship among ball behavior, injection and initial spray characteristics of ultra-high pressure GDI injector, *Fuel* 285, 119089 (2021). https://doi.org/10.1016/j.fuel.2020.119089.
- [47] Wang J, He, Z, Duan L, Zhou H, Zhong W, et al., Effect of diesel/gasoline/HCB blends and temperature on string cavitating flow in common-rail injector nozzle, Fuel 304, 121402 (2021). https://doi.org/10.1016/j.fuel.2021.121402.
- [48] Jahanbakhshi A, Karami-Boozhani S, Yousef M & Ooi J B, Performance of bioethanol and diesel fuel by thermodynamic simulation of the miller cycle in the diesel engine, *Result Eng*, 12, 100279 (2021). https://doi.org/10.1016/j.rineng.2021.100279.
- [49] Wei S, Zhao X, Liu X, Qu X, He C, *et al.*, Research on effects of early intake valve closure (EIVC) miller cycle on combustion and emissions of marine diesel engines at medium and low loads, *Energ*, 173, 48-58 (2019). https://doi.org/10.1016/j.energy.2019.01.110.

- [50] Zhou S, Gao R, Feng Y & Zhu Y, Evaluation of Miller cycle and fuel injection direction strategies for low NOx emission in marine two-stroke engine, *Intern JHydrogen Energ*, 42 (31), 20351-20360 (2017). https://doi.org/10.1016/j.ijhydene.2017.06.020.
- [51] Gonca G& Sahin B, Effect of turbo charging and steam injection methods on the performance of a Miller cycle diesel engine (MCDE), *Appl ThermEng*, 118, 138-146 (2017). https://doi.org/10.1016/j.applthermaleng.2017.02.039.
- [52] Jain A, Singh A P& Agarwal A K, Effect of split fuel injection and EGR on NO_x and PM emission reduction in a low temperature combustion (LTC) mode diesel engine, *Energ*, 122, 249-264 (2017). https://doi.org/10.1016/j.energy.2017.01.050.
- [53) Li Y, Peng J, Shi Z & Xu R, Effects of split injection strategy on the combustion, emission and economic performance of the low-octane gasoline fueled MPCI engines, *Energ Rep*, 7, 6651-6657 (2021). https://doi.org/10.1016/j.egyr.2021.09.156.
- [54] How H G, Masjuki H H, Kalam M A & Teoh Y H, Influence of injection timing and split injection strategies on performance, emissions, and combustion characteristics of diesel engine fueled with biodiesel blended fuels, *Fuel* 213, 106-114 (2018). https://doi.org/10.1016/j.fuel.2017.10.102.
- [55] Marchitto L, Calabria R, Tornatore C, Bellettre J, Massoli P, et al., Optical investigations in a CI engine fueled with water in diesel emulsion produced through microchannels, Exp Therm Fluid Sci, 95, 96-103 (2018). https://doi.org/10.1016/j.expthermflusci.2018.02.008.
- Vigneswaran R, Balasubramanian D &Sastha B D S, Performance, emission and combustion characteristics of unmodified diesel engine with titanium dioxide (TiO₂) nano particle along with water-in-diesel emulsion fuel, *Fuel*, 285, 119115 (2021). https://doi.org/10.1016/j.fuel.2020.119115.
- [57] Ithnin A M, Noge H, Kadir H A & Jazair W, An overview of utilizing water-in-diesel emulsion fuel in diesel engine and its potential research study, *J Energ Inst*, 87 (4), 273-288 (2014). https://doi.org/10.1016/j.joei.2014.04.002.
- [58] Jiaqiang E, Zhang Z, Chen J, Pham M, Zhao X, et al., Performance and emission evaluation of a marine diesel engine fueled by water biodiesel-diesel emulsion blends with a fuel additive of a cerium oxide nanoparticle, Energ ConvManage, 169, 194-205 (2018). https://doi.org/10.1016/j.enconman.2018.05.073.
- [59] Hasannuddin A K, Yahya W J, Sarah A, Ithnin A M, Syahrullail S, et al., Performance, emissions and carbon deposit characteristics of diesel engine operating on emulsion fuel, Energ, 142, 496-506 (2018). https://doi.org/10.1016/j.energy.2017.10.044.
- [60] Abu-Zaid M, Performance of single cylinder, direct injection Diesel engine using water fuel emulsions, *Energ ConveManage*, 45 (5), 697-705 (2004). https://doi.org/10.1016/S0196-8904(03)00179-1.
- [61] Hosseinzadeh-Bandbafha H, Tabatabaei M, Aghbashlo M & Shojaei T R, Methods of using water additive and its Effect on performance and emissions of diesel engine, *Zanco J Pure ApplSci*, 31(s3), 69-74 (2019). https://doi.org/10.21271/ZJPAS.31.s3.10.
- [62] Nour M, Sun Z, El-Seesy A I & Lia X, Experimental evaluation of the performance and emissions of a direct-injection compression-ignition engine fueled with n-hexanol–diesel blends, *Fuel*, 302, 121144 (2021). https://doi.org/10.1016/j.fuel.2021.121144.

- [63] Busuttil D, Camilleri G & Farrugia M, Mechatronics for water injection in SI engine, *Proceedings of the 16th International Conference on Mechatronics Mechatronika* 2014, 308-313 (2014). https://doi.org/10.1109/MECHATRONIKA.2014.7018276.
- [64] Mingrui W, Sa N T, Turkson R F, Jinping L & Guanlun G, Water injection for higher engine performance and lower emissions, *JEnerg Inst*, 90 (2), 285-299 (2017). https://doi.org/10.1016/j.joei.2015.12.003.
- [65] Arabaci E &İçingür Y, Thermodynamic investigation of experimental performance parameters of a water injection with exhaust heat recovery six-stroke engine, *J EnergInst*, 89 (4), 569-577 (2016). https://doi.org/10.1016/j.joei.2015.06.006.
- [66] Merkisz J & Waligórski M, Strategy of the combustion process diagnosis in direct injection engines, *Procedia Eng*, 96, 294-301 (2014). https://doi.org/10.1016/j.proeng.2014.12.141.
- [67] Liu Z, Sun P, Du Y, Yu X, Dong W, et al., Improvement of combustion and emission by combined combustion of ethanol premix and gasoline direct injection in SI engine, Fuel 292, 120403 (2021). https://doi.org/10.1016/j.fuel.2021.120403.
- [68] Tauzia X, Maiboom A & Shah S R, Experimental study of inlet manifold water injection on combustion and emissions of an automotive direct injection diesel engine, *Energ*, 35 (9), 3628-3639 (2010). https://doi.org/10.1016/j.energy.2010.05.007.
- [69] Kökkülünk G, Gonc G, Ayhan V, Cesur I & Parlaka A, Theoretical and experimental investigation of diesel engine with steam injection system on performance and emission parameters, *App Therm Eng*, 54 (1), 161-170 (2013). https://doi.org/10.1016/j.applthermaleng.2013.01.034
- [70] Sun X, Liu H, Duan X, Guo H, Li Y, *et al.*,Effect of hydrogen enrichment on the flame propagation, emissions formation and energy balance of the natural gas spark ignition engine, *Fuel*, 307, 121843 (2022). https://doi.org/10.1016/j.fuel.2021.121843.
- [71] Masoud D, Ghafourizadeh M & Schneider G, The Formation of Pollutants CO/CO₂ in a Steam-Injected Combustor, (2018). https://doi.org/10.11159/FFHMT18.137.
- [72] Zhu S, Hu B, Akehurst S, Copeland C, Lewis A, et al., A review of water injection applied on the internal combustion engine, Energ Conv Manage, 184, 139-158 (2019). https://doi.org/10.1016/j.enconman.2019.01.042.
- [73] Wei M, Nguyen T S, Turkson R F, Guo G & Liu J, The Effect ofwater injection on the control of in-cylinder pressure and enhanced power output in a four-stroke spark-ignition engine, *Sustainability*, 8, 993 (2016). https://doi.org/10.3390/su8100993.
- [74] Fengyu G, Tang X, Yi H, Zhao S, Li C, et al., A review on selective catalytic reduction of nox by nh3 over mn–based catalysts at low temperatures: catalysts, mechanisms, kinetics and DFT calculations, Catalysts, 7 (7), 199 (2017). https://doi.org/10.3390/catal7070199.
- [75] Praveena V & Martin M L J, A review on various after treatment techniques to reduce NO_xemissions in a CI engine, *J Energ Inst*, 91 (5), 704-720 (2018). https://doi.org/10.1016/j.joei.2017.05.010.
- [76] Winnes H, Fridell E & Moldanová J,Effects of marine exhaust gas scrubbers on gas and particle emissions, *JMar SciEng*, 8 (4), 299 (2020). https://doi.org/10.3390/jmse8040299.
- [77] Wu S, Kuang M, Zhao M, Yang G, Geng X,et al., ASPEN PLUS desulfurization simulations for the scrubber of a large-scale marine diesel engine: main scrubbing section's desulfurization share optimization and superiority confirmation for the seawater/seawater cascade-scrubbing solution, EnviSciPollut Res, 28 (17), 22131-22145 (2021).

- [78] Vedachalam S, Baquerizo N & Dalai A K, Review on impacts of low sulfur regulations on marine fuels and compliance options, *Fuel*, 310 (part A), 122243 (2022). https://doi.org/10.1016/j.fuel.2021.122243.
- [79] Zhu M, Li K X, Lin K C, Shi W & Yanga J, How can shipowners comply with the 2020 global sulphur limit economically?, *Transport Res Part D: Transport Environ*, 79, 102234 (2020). https://doi.org/10.1016/j.trd.2020.102234.
- [80] Jiang L, Kronbak J & Christensen L P, The costs and benefits of sulphur reduction measures: Sulphur scrubbers versus marine gas oil, *Transport Res Part D: Transport Environ*, 28, 19-27 (2014). https://doi.org/10.1016/j.trd.2013.12.005.